

# Novel Approach to Creation of Portable Self-Propelled Autonomous Massage Robots with Triangular and Octahedral Parallel Structures

SERGEY SAYAPIN<sup>1, 2</sup>

<sup>1</sup>The Department of vibration biomechanics

The Institute for Machine Science named after A.A. Blagonravov of the Russian Academy of Sciences  
4 Maly Kharitonyevsky Pereulok, Moscow, 101990, Russia

<sup>2</sup>The Department of Theoretical Mechanics

The Bauman Moscow State Technical University  
2-nd Baumanskaya, 5, Moscow, 105005, Russia

RUSSIA

S.Sayapin@rambler.ru

ELENA SAYAPINA

The Department of transfusion medicine

The A. Tsyb Medical Radiological Research Centre – branch of the National Medical Research  
Radiological Centre of the Ministry of Health of the Russian Federation  
10 Zhukov st., Obninsk, Kaluga region, 249036, Russia

RUSSIA

E.Sayapina@rambler.ru

*Abstract:* - In this paper, a novel approach to a creation of self-propelled autonomous portable massage robots based on original 2D and 3D parallel mechanisms is presented. A 2D massage robot based on a triangular parallel structure with 3 d.o.f., called a Triangle, is designed for a sliding cupping-glass massage of back and chest. A 3D massage robot based on an octahedral parallel structure with 12 d.o.f., called an Octahedral dodekapod, is designed for a massage of neck, upper and lower extremities, including knee and elbow joints. Benefits of the Triangle and the Octahedral dodekapod with respect to anthropomorphic robots with one or two arms are outlined, along with possible applications for an autonomous massage.

*Key-Words:* - massage robots, self-propelled portable masseurs, 2D and 3D parallel robots, modular robot, rehabilitation robots

## 1 Introduction

It is known that a massage is now considered one of the most effective non-drug methods of effective means of disease prevention, treatment, rehabilitation, removal of weariness. Therefore now massage is used in clinics, hospitals, and medical centers of many countries. All kinds of the massage are made by a masseur or a patient (self-massage) manually or by massage apparatuses [1]. In order to augment an effect of traditional manual techniques, the masseur may use other massage techniques, for example, such as a sliding cupping-glass massage (SCGM) for back and chest. However, usually SCGM is independent kind of manual massage including combination influences to patient's back and chest by the cupping-glasses and massage. There are numerous examples of effective using of SCGM in practice medicine [1]. In Fig. 1 (a) basic massage movements for SCGM by vacuum massage

cupping glass (VMCG) are shown. These movements include following: I - straight, II - zigzag, III - spiral, and IV - figure-of-eight. The masseur makes the massage personally. Therefore the presence of the masseur is required, but he can make the massage only with one patient by two hands. As a result a daily productivity of the masseur is limited. Moreover, the masseur usually performs laborious and monotonous manipulations all day long that lead to his fatigue. A work of the masseur is connected with a big physical stress that can be cause of pathological changes in spine and lumbar one. The self-massage also demands from patient of the big physical stress that is inadmissible for separate categories of patients. Therefore labor-intensive procedures of the massage should be robotized.

Similar problems exist when you massage the upper and lower extremities, including massage of

the elbow and knee joints, and also neck of the patients.

Currently, there are variable robots, which can be used as base of half-autonomous or autonomous massage robots, for example, such as

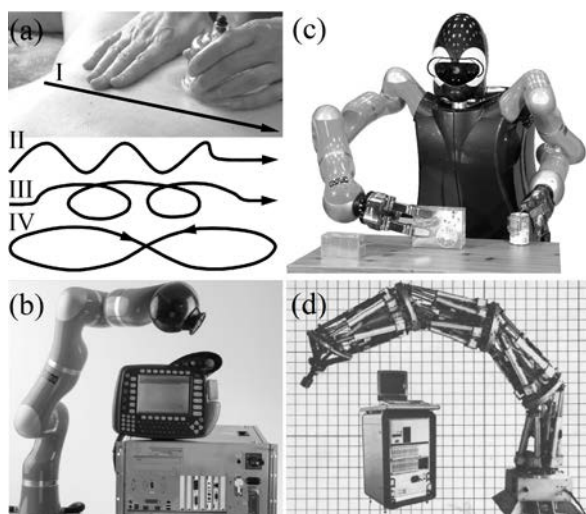


Fig. 1. Basic massage movements by VMCG (a); the KUKA lightweight robot with controller (b); mobile dual arm robot with 3-finger hands (c); the multi-module parallel robot Logabex LX4 (d)

anthropomorphic one/two-armed robots (similar to the KUKA lightweight robot) [2] or multi-module parallel robots (similar to the Logabex robot LX4) [3], which are shown in Fig. 1 (b, c, and d).

Unfortunately, now there are only few examples of practical use of anthropomorphic one-armed massage robots which was created similar to the industrial robots [4]-[6]. However, these one-armed robots have large sizes and weight, and therefore, they cannot be used in carried massage robotic systems. Furthermore, in case of the patient's body movements, the programmed motion of massage robot is not suitable. Thus, a creation of the carried massage robots for SCGM for back and chest being able to work autonomously without the presence of the masseur is an urgent task. Therefore modern rehabilitation medicine is needed of advanced intelligence carried massage robots, being able to work autonomously without the presence of the masseur. I propose new concepts of self-propelled multifunctional intelligence autonomous carried massage robot for SCGM for back and chest based on a triangular parallel structure with 3 d.o.f., called the Triangle [7], and massage robot for massage of the upper and lower extremities, including massage of the elbow and knee joints, and neck based on a octahedral parallel structure with 12 d.o.f., called the Octahedral dodekapod [8]. The description of design principles of the Triangle and the Octahedral

dodekapod as future intelligence base blocks for various rehabilitation and other robotic systems that can self-propelled and self-reconfigure is presented below.

## 2 Description of Triangle

The Triangle is based on the 2D triangular parallel mechanism and therefore it has higher a specific stiffness and a bearing capacity, and lower specific weight. In Fig. 2 a structural scheme of the Triangle is shown. The proposed concept will allow be robotize the process of SCGM. As a result there are the following advantages:

1) The Triangle is able to organize autonomous conduction of SCGM to several patients simultaneously, and holding cupping massage by several vacuum massage cupping-glasses (VMCG) in the sitting or standing, for example by three VMCG on chest and three VMCG on back of patient at the same time and, as a result the daily productivity of the masseur increases.

2) There is massage by sliding and stretching of muscle tissues at the same time the three VMCG that improves the performance of the process of massage.

3) There is the autonomous SCGM to hard reached areas of the body such as back, and ensure the controlled movement of VMCG and VMCG bypass the moving parts of body that are not valid for massage effects, such as moles, sensitive and damaged skin, post-operative wounds, etc.

4) The autonomous SCGM does not require special facilities and can be performed at the bedside and at the home.

5) The Triangle released extra time, which can be used to conduct other types of massage and, as a consequence, there is a possibility of increasing the number of patients served per shift.

6) There is the reduction of the physical fatigue of the masseur, thereby increasing his productivity and improving health at the end of the work shift.

The Triangle (Fig. 2) has a massage device based on the active triangular module **ABC** with the parallel structure. The sides **AB**, **BC** and **CA** are made in the form of similar rods. The ends of rods are pivotally connected at the vertices of the active triangular module **ABC** with the VMCG 1. Thus, each of the rods is provided a linear drive 2, a force sensor 3, a relative-displacement sensor 4, and a relative-velocity sensor 5. All vertices of triangle module **ABC** are executed with possibility of connection the like rods through them 2 for the

formation of the additional active triangular parallel structures.

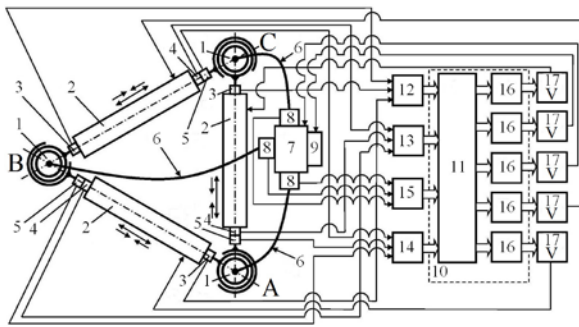


Fig. 2. Structural scheme of Triangle

Each of VMCG 1 is pivotally connected at the vertices of the active triangular module **ABC** and forms its device discrete fixation to the patient's body. In addition, each of the VMCG 1 is hermetically connected by a flexible hose 6 to a mated canal of an air distributor 7 of a degassing system provided with a pressure sensor 8, the air distributor 7 and a vacuum pump 9 electrically connected to a control system 10 in the form of a neural computer 11 with digital-to-analogue converters (DAC), and relevant software (the main advantages of neural computer are associated with massively parallel processing, and as the result is high speed, low requirements for stability and accuracy of the parameters of the elementary nodes, resistance to interference and destruction). The inputs of the control system 10 are connected through the data buses of analog-digital converters (ADC) to the outputs: of ADC 12, 13, 14 and 15 of the force sensors 3 for ADC 12; the relative-displacement sensors 4 for ADC 13; the relative-velocity sensors 5 for ADC 14; and the pressure sensors 8 for ADC 15. The outputs of the control system 10 are connected through the output data buses to the corresponding inputs of software and the following units, connected in series: DAC 16, power amplifiers 17, linear drives 2, air distributor 7, and vacuum pump 9. The control system 10 made with the possibility of operational control and management in real-time.

The Triangle works as follows. On surface of the patient's body [1] an active triangle module **ABC** applied with VMCG 1 in its vertices (Fig. 3, a, b). The initial position of the active triangle module **ABC** is mounted on the massaged area of the patient's body arbitrary. Then the VMCG 1 degas by the vacuum pump 9 (Fig. 2) and after their individual suction and retraction of the skin on the value for reliable fixation of VMCG 1 and excluding injury of the patient's skin, which is determined visually, close the corresponding valve

(in the figures not shown) of the air distributor 7 and record the value of the minimum allowable pressure with pressure sensors 8.

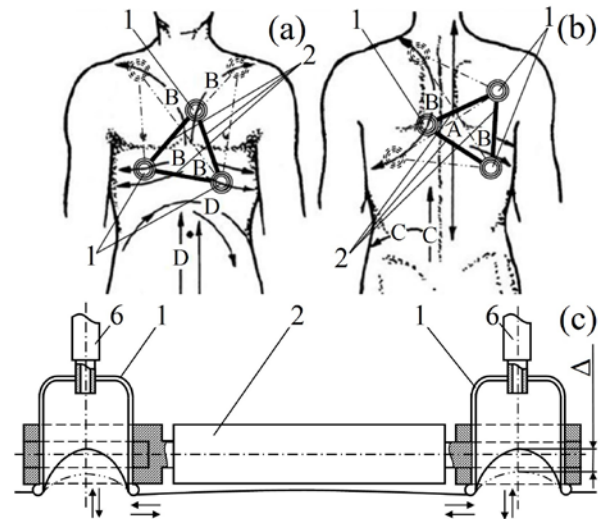


Fig. 3. Schemes of installation of Triangle and its massage movements in the front view (a) and rear (b); scheme of the local vacuum-massage and the massage by displacement and stretching the muscles through the massager (c)

Then, using the appropriate valves (on the pictures conventionally are not shown) of the air distributor 7 is produced depressurization of VMCG 1 to the maximum pressure inside them, which ensures the possibility of their sliding mobility according to the patient's body without detachment from him. At this point, these valves of the air distributor 7 and with the help of pressure sensors 8 are fixed values, the maximum allowable pressures inside the VMCG 1. Further, control system 10 enters data, which include the contours of body areas massaged, associated with the base coordinate system and the coordinates of the areas of the body that are not valid for massage effects, such as moles, sensitive and damaged skin, surgical wound, etc. Then the control system 10 gives the command to the vacuum pump 9 and the air distributor 7 to degas through the flexible hoses 6 and the respective valves of the air distributor 7 two fixed VMCG 1 on surface of the patient's body and one sliding VMCG. After reaching in these fixed and sliding VMCG the minimum allowable and maximum allowable pressures from the respective pressure sensors 8 through the ADC 15 receives analog signals into the control system 10 in which the control commands are formed, which through the corresponding DAC 16 and power amplifier 17 are fed to the closure of the valves of the air distributor 7 and the shutdown of the vacuum pump 9. After that, relative to the base coordinate system entering coordinates of the centres of the two fixed VMCG and one sliding VMCG and the distance between them. Then, the

masseur gives a command to perform the programmed massage movements for the sliding VMCG.

In Fig. 3 (a, b) schemes of the SCGM in various diseases are shown: spinal osteochondrosis and lumbago (A); pneumonia and bronchitis (B); myositis and sciatica (C); colitis and hypertension (D) [1]. As we can see in the above diseases impose the straight movements of the one sliding VMCG 1 and its movements along the circular arcs. After receipt of the command to the control system 10 in the computer 11 (taking into account the previously entered data) the initial coordinates of the VMCG 1 for carrying out massage movements of the VMCG 1 are calculating, for example arcuate movements (B) (Fig. 3, a, b), from the condition of ensuring a minimum number of VMCG rearrangements required to convert the selected path of movement, which depend on the maximum strokes of the linear drives 2. The active triangle module **ABC** can be installed in the initial position in such way that each of his VMCG 1 will be able to alternately perform the rolling massage movement on different trajectories of the movements of b without its permutations (Fig. 3, b). The movement of the VMCG 1 on the surface of the patient's body is carried out by appropriately changing the lengths of the linear drives 2, controlled relative-displacement sensor 4. Thus the required speed of the massage movements of the VMCG 1 on the patient's body is provided by the speed control of axial movements of the linear drives 2 according to signals from the respective relative-velocity sensors 5. The geometric resistance of the active triangular module **ABC** (Fig. 3) allows you to define the coordinates of its vertices **A**, **B** and **C** by measuring by the relative-displacement sensor 4 of the lengths of all rods and control their movements similarly to the organization of spatial movements of the *I*-coordinate manipulator [9]. The relative-velocity sensor 5 allow to control the speed of movement of the sliding VMCG 1 at this stage of massage in accordance with the valid values, defined for this type of massage movements and introduced to the control system 10. It should be noted that all of the VMCG 1 in the course of their rearrangements through sliding motions on the massaged surface of the patient body, alternately become floating and unmoveable. Here in, the process of their permutation. In the active triangular module **ABC** one of the VMCG 1 closest to his move) and the other two are roaming and unmoveable, respectively. While the maximum allowable air pressure sets in one roaming sliding VMCG, and in two fixed VMCG – minimum allowable air

pressure. After that, the control system is commanded to switch on the linear drives 2, is connected to the sliding VMCG 1 and produced a consistent change in their lengths at a given speed controlled by the relative-speed sensor 5. After moving the sliding VMCG 1 to a specified destination (or intermediate) point, determined by the relative-displacement sensor 4 associated with linear drive 2, the command is made to switch them off. Then displacement of the sliding VMCG becoming the fixed VMCG, and one of the two fixed VMCG is becoming roaming. The pressure in the displaced VMCG is the minimum, and another is allowable maximum. Further, similar to the previous cycle from the control system is commanded to switch on the linear drive 2, is connected to the moving VMCG and produced a consistent change in their lengths at a given speed controlled by the relative-speed sensor 5. Then similarly do the movement of third VMCG in final or intermediate point. After displacement of all VMCG in the calculation the initial coordinates two of the VMCG are made unmoveable, and the third lying on the trajectory massage movements, for example the arc **B** (Fig. 3, b), make sliding cupping-glass and make her massage movements. Thus, depending on the desired massage motions, the estimated initial coordinates of VMCG can be computed in such way that all VMCG will be on the trajectories required of massage movements, for example on the arcs **B** (Fig. 3, b). In this case, the massage can be performed sequentially and alternately. Permutations of triangular **ABC** module can be arranged in such way that the trajectory of all movements VMCG will coincide with the specified trajectory of massage movements in the process of permutations, i.e. there will not be "spurious" passages of VMCG.

Using the Triangle it's also able to produce a local vacuum massage and the massage by sliding and stretching of the muscle tissue [1]. In Fig. 3 (c) the scheme of their conduct is shown. Local vacuum massage is performed at a fixed on the patient's body VMCG 1 by the vacuum in the air up to a pressure whose value is in the range from the maximum pressure to the minimum pressure. For its implementation by commands from the control system in the VMCG with established frequency and amplitude of the pressure change from the minimum permissible to the maximum and Vice versa. Management of alternate higher and lower pressure is carried out using the diffuser 7 and vacuum pump 9 according to the commands from the control system 10, formed as a result of processing the signals from the pressure sensors 8.

The distance between the involved skin surface at the maximum pressure inside the jar and the involved skin surface with minimal pressure is  $\Delta$  (Fig. 3). The distance  $\Delta$  corresponds to the maximum value of the amplitude in the conduct to local vibration by varying the pressure in the VMCG.

Massage by sliding and stretching the muscle tissues is produced, while still fixed on the patient's body VMCG 1 by discharging air to the minimum allowable pressure. It is possible to carry out this type of massage as alternate movement of the linear actuators, as the simultaneous movement of two or more linear actuators. After fixing the VMCG 1 on the massaged area of the body of the patient (Fig. 3) at the position at which the length of the linear actuator 2 correspond to their average values, the control system 10 is commanded to the linear drive 2 on decrease (increase) its length at a predetermined value, after reaching which the linear actuator 2 is stopped and is switched on for reverse, increasing (decreasing) its length to a set value. The process is repeated at a given rate, the required number of cycles. The maximum change in length of the linear actuator 2 corresponds to a given vibration amplitude of the massage movements of compression-tension. Changing the length of the linear actuator 2 and the amplitude are controlled by the relative movement of the sensor 4 and the speed – with the help of relative velocity sensor 5. The efforts of the mechanical effects of VMCG 1 on the muscle tissue of the patient performing all types of massage are controlled by the force sensor 3. In case of exceeding the set value of the effort in conducting a moving cupping massage, on command from the control system 10 produces an increase in pressure in the VMCG 1 by the amount of the established step and take him for the maximum allowed pressure value and continue massage. In case of exceeding a predetermined force value during the massage by sliding and stretching of muscle tissue, control system 10 reduces the magnitude of the amplitude which is set by the permissible forces in the extreme positions of the linear actuator 2 and continue the massage.

In case of spontaneous detachment of one of vacuum massage cupping-glasses from the patient's body during the massage unplanned increase in her pressure happens, as in the control system 10 receives the corresponding signal from the pressure sensor 8. In response to the situation the control system 10 will give the appropriate command to the distributor valve 7 and vacuum pump 9. It should be noted that the active triangular bearing module **ABC** on the massaged area of the body of the patient

occurs at three points in the form of VMCG 1. Therefore, in the case of the horizontal position of the patient gravity from 1/3 the weight of the active triangle module **ABC** will be enough for a snug fit to the surface of the seal body VMCG 1 and subsequent suction to the body after lowering the pressure to the minimum allowable value. This will mean that the VMCG 1 is recorded on the patient's body and the massage will continue in accordance with the established program. In case of the pressure decrease in the cupping-glass is not going to happen, from the control system 10 will receive the signal about the movement of the VMCG to a new location and repeat the procedure vacuum. And, in case of repeated unsuccessful attempts, from the control system 10 the massage therapist will receive the signal about emergency situation, for correction of which requires his involvement. After the liquidation of the emergency situation massage therapist, the massage procedure will be continued offline.

We implemented the Triangle concept with a real pneumatic prototype that uses nine syringes (60.0 ml) and three barrels (60.0 ml) as three linear pneumatic actuators with three pneumatic pumps and as three VMCG with three vacuum pumps (Fig. 4, a). The pneumatic prototype is operated manually.

We also performed locomotion experiments and

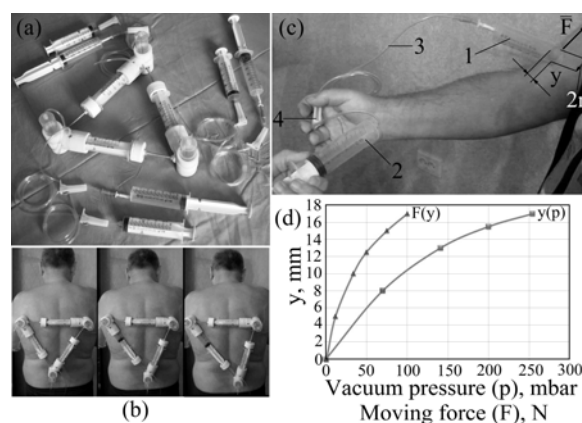


Fig. 4. The pneumatic prototype of the Triangle (a); SCGM of the back by the pneumatic prototype of the Triangle (b); the prototype of the VMCG (c); the experimental relationships between (y) and (p), and (F) and (y) for the prototype of the VMCG (d)

SCGM of the patient's back by the pneumatic prototype (Fig. 4, b). In Fig. 4 (c) a prototype of VMCG is shown, which consists of one barrel 1, one syringe 2, and tubing 3 with a roller clamp 4 of an infusion system. This prototype is the same as VMCG with vacuum pump of the real pneumatic prototype (Fig. 4, a, b). Fig. 4 (d) illustrates the experimental relationships between skin uplift (y)

and a vacuum pressure ( $p$ ), and also between skin uplift ( $y$ ) and moving force ( $F$ ). Fig. 4 (d) also illustrates the relationship between moving force ( $F$ ) and vacuum pressure ( $p$ ). In the experiments, vacuum pressure loadings applied using the prototype of VMCG was subjected to the male's shoulder skin in the 60 year age range. The experiments were conducted by gently pressing barrel 1 of diameter 29.0 mm against the skin to ensure a good initial contact and then activating syringe 2 (vacuum pump) to create the vacuum inside the barrel of syringe 2 so that the skin is drawn into the barrel 1 (Fig. 4, c). The bulging of the skin as a result of cupping is shown in Fig. 4; all images were captured using a Canon digital camera IXUS 990 15. Moving forces ( $F$ ) were measured using the Dynamometer 5029 DPU-0.1-2 (GOST 13837-79). The vacuum pressures ( $p$ ) developed inside the prototype of VMCG were calculated using Boyle's Law:

$$p_i V_i = p_f V_f,$$

where the subscripts  $i$  and  $f$  refer to initial (before pumping,  $p_i=1000$  mbar) and final (after pumping) states and measured volumes of barrel 1 (prototype of VMCG, 60.0 ml) with tubing 3 (3.18 ml) and barrel (60.0 ml) of syringe 2 (vacuum pumping chamber) which is decreased by volume of skin uplift ( $V_{su}$ ). The volumes of skin uplift (Fig. 4, c) were calculated as volumes of ball segment ( $V_{su} = \pi y^2 (3r - y)/3$ ).

### 3 Other Kinds Locomotions of Triangle

The Triangle can locomote also without vacuum pressure using other types of locomotion, for example, such as a leopard crawl (Fig. 5, a), a vertical rolling (similar to the tetrahedral walker movement) [10], and a shuffle (Fig. 6).

The leopard crawl (Fig. 5, a) can be used when locomotion of the Triangle on a horizontal or inclined surface.

The Triangle can shuffle one's feet when moving in a vertical plane as shown in Fig. 6. The movement cycle of the Triangle includes following stages: initial position (a), a displacement of the center of gravity left (b), forward translation of right joint by using the shuffle (c), the displacement of the center of gravity right (d), forward translation of left joint by using the shuffle (e), final/initial position (a). Also the pneumatic prototype of the

Triangle can be rotated by the plunger installed in right or left prototype of the VMCG (f).

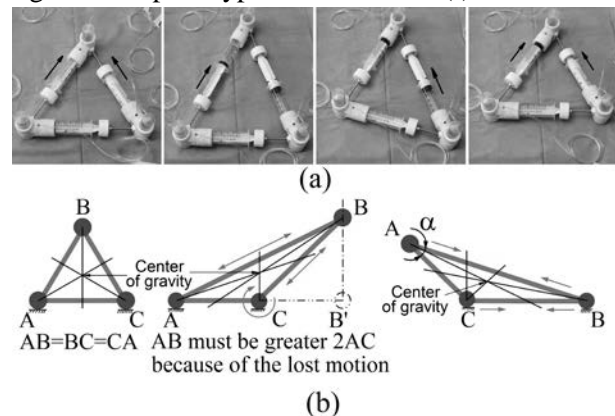


Fig. 5. Locomotion of the Triangle by using the leopard crawl (a) and the vertical rolling (b)

The locomotion of the Triangle in the vertical plane (Fig. 5, b and Fig. 6) can be used when movement in narrow aisles, for example between the walls. The angle  $\alpha$  is chosen based on design parameters of the Triangle.

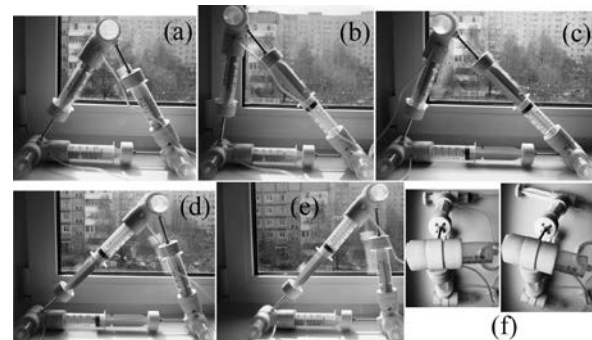


Fig. 6. The movement cycle of the Triangle by using the shuffle (a-e) and the ability of rotation (f)

### 4 Description of Octahedral Dodekapod

The Octahedral dodekapod is modern stage of development in the field of parallel spatial robots and it based on an active octahedral parallel structure with 12 d.o.f. Such robot versus hexapod has the larger workspace. Each of its sides can clamp (unclamp) things with a closed loop surface of various form. Reference [11, 12] shows new functional capabilities of dodekapod, such as the self-movement, the diagnostics of contact surfaces, and other ones. They were used us in adaptive parallel spatial self-propelled modular robot, called the Octahedral dodekapod [8], for medical applications, such as the self-moving masseur for the upper extremities and the lower ones, the exoskeleton of the forearm with the elbow joint and

that of the lower leg with the knee joint which may be used in various fields of rehabilitative medicine.

The schematic view of the octahedral module of the Octahedral dodekapod (a) and the simplified structural scheme of the control system (b) are shown in Fig. 7. The structural scheme includes maximal number of sensors, radial stops and clamps. This number depends on the applications and it may be decreased. The Octahedral dodekapod is executed as the octahedral module 1.

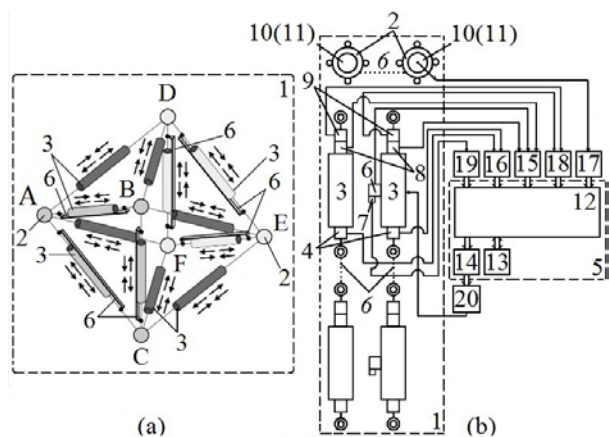


Fig. 7. The schematic view of the octahedral module of the Octahedral dodekapod (a) and the simplified structural scheme of the control system (b)

All ribs of the octahedron are executed as the rods with the linear drives 2 each of which have the axial force sensor 3, the medial force sensor 4, the relative linear movement sensor 5, and the relative velocity sensor 6. The ends of the adjacent ribs are connected by the spherical joints in the tops 7 of the octahedral module 1. The tops 7 contain the radial stops and the middles of the rods contain the clamps (on Fig. 7 were not shown) each of which have the temperature sensor 8. The octahedral module 1 is a spatial farm as soon as all linear drives 2 are turned off. All tops 7 have the spatial position sensors 9 which are integrated with the three-axial blocks of the accelerometers 10. The control system (CS) 11 includes: the neurocomputer (NC) 12, the software 13 and the digital-analogue integrated converters (DAIC) 14. The entrances of CS 11 are connected to exits of the analogue-digital integrated converter (ADIC) 15

for the force sensors 3 and 4, ADIC 16 for the relative linear movement sensors 5, ADIC 17 for the spatial position sensors 9 with the three-axial blocks of the accelerometers 10, ADIC 18 for the relative velocity sensors 6, and ADIC 19 for the temperature sensors 8. Exits of CS 11 are connected to entrances of the software 13 and DAIC 14. The exits DAIC 14 are connected to the power amplifier 20 which is connected to each of the linear drives 2.

The octahedral module 1 may be used as a base

element not only at the single-modular Octahedral dodekapod, but also at the multimodular ones. The radial stops and the clamps (on Fig. 7 were not shown) provide the transmission of the efforts from linear drives toward the internal and external contact surfaces. The force sensors 3, 4 and temperature sensors 8 provide the operative control of these efforts and temperature in the contact places. The spatial position sensors 9 with three-axial blocks of the accelerometers 10 provide the operative control of the spatial position of tops 7 and of vibration along each of axes of rods with linear drives 2. The relative linear movement sensors 5 and the relative velocity sensors 6 (observers of conditions) of the linear drives 2 register their relative movements and velocities. Before using it we will have to place the octahedral module 1 in inside or outside of the closed surface and then carry out the necessary movements depending on tasks. The linear drives 2 and the control systems 11 fulfill the coordinated changes of the lengths of the ribs of the octahedral module herewith. As a result the tops 7 have got spatial movement concerning a base system of coordinates. A geometrical invariability of the octahedral module 1 allows to define the spatial coordinates of all tops 7 as a result of the measurement of the lengths of all rods and to control their spatial movements similarly to the organization of spatial movements of the  $I$ -coordinate manipulator [9] The sensors of the spatial position 9 allow elevating a precision of these measurements herewith. The NC 12 and the software 13 provide the control of real time.

The self-propelled masseur (SPM) is based on the use of the Octahedral dodekapod without mounting of the axial force sensors 3 (Fig. 7), the temperature sensor 8 and the radial stops of the tops 7, and the claps of lateral sides of the octahedral module 1. The SPM may be used to do the massage of the upper extremities and the lower ones.

The self-propelled of SPM on the arm is shown in Fig. 8 and it includes the following stages.

1) Initial Stage or Position 1, 2, 7: It is the placement of SPM on the column (a) or on the arm (b) (Fig. 8). The rods AB, BC, AC, DE, EF, and DF are shortened by the linear drives 2. These drives will be stopped by CS 11 from signals of the force sensors 4 (Fig. 7, Fig. 8).

2) Stage 1 or Position 3: The rods DE, EF, and DF are lengthened by the linear drives 2. These drives will be stopped by CS 11 from signals of the relative linear movement sensors 5.

3) Stage 2 or Position 4: The rods AD, AF, BD, BE, CE, and CF are lengthened by the linear drives 2. These drives will be stopped by CS from signals

of the relative linear movement sensors 5.

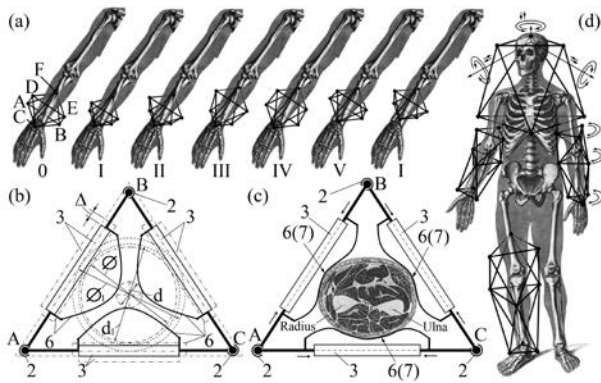


Fig. 8. The self-movement of SPM on the arm (a), a geometrics of grasping face (b) and pressing arm (c), the exoskeletons (d)

4) Stage 3, 4 or Position 5: The rods DE, EF, and DF are shortened by the linear drives 2. These drives will be stopped by CF 11 from signals of the force sensors 4. The rods AB, BC, and AC are lengthened by the linear drives 2. These drives will be stopped by CS 11 from signals of the relative linear movement sensors 5.

5) Stage 5 or position 6: The rods AD, AF, BD, BE, CE, and CF are shortened by the linear drives 2. These drives will be stopped by CS 11 from signals of the relative linear movement sensors 5.

6) Initial Stage or Position 7: The rods AB, BC, AC, DE, EF, and DF are shortened by the linear drives 2. These drives will be stopped by CS 11 from signals of the force sensors 4.

7) Position 8: It is the initiation of next a cycle. The rods DE, EF, and DF are lengthened by the linear drives 2. These drives will be stopped by CS 11 from signals of the relative linear movement sensors 5. The rods AD, AF, BD, BE, CE, and CF are lengthened by the linear drives 2. These drives will be stopped by CS 11 from signals of the relative linear movement sensors 5.

SPM has 12 d.o.f. and it may therefore be used for massage operations such as stroking, friction, malaxation, and vibration on all surfaces of upper extremities and the lower ones. The interest of this concept is that it can be fully automated. The temperature sensors 8 permit to measure the temperature of body. The three-axial blocks of the accelerometers 10 may be used not only for remote monitoring of the vibration influences, but also for the pulse.

SPM may also be used for a limitation of an articular mobility and for a decrease of compressive (extending) load. The contact places may be changed to decrease stagnant effects.

The octahedral modules 1 (Fig. 7, a) can connect together, forming some new mobile structures for

various applications. For example two octahedral modules can be connected together, forming exoskeleton of the forearm with the elbow joint and that of the lower leg with the knee joint. These exoskeletons are shown in Fig. 9. They are based on the use of the octahedral modules without mounting of the temperature sensor 8 and the radial stops of the tops 7, and the claps of lateral sides of the octahedral module 1 (Fig. 7).

This concept possesses the following functional capabilities and the diagnostic ones.

1) Adaptation: These exoskeletons can adapt to the arm (leg) with different sizes. The common side of two octahedral modules 1 can change sizes and it increases the workspace for the elbow (knee) joint.

2) Forced Movement: These exoskeletons can be used for the forced movements of the forearm with the elbow joint and that of the lower leg with the knee joint in full compliance with the program of rehabilitation.

3) Force-Moment Measurements: The force sensors 3, 4 may be used for the force-moment measurements of arm (leg).

4) Remote Monitoring: It may be used with the relative linear movement sensors 5, and the relative velocity sensors 6, the spatial position sensors 9, the three-axial blocks of the accelerometers 10 for the monitoring of arm (leg) movements and vibration influences.

## 5 Conclusion

Any suitable self-propelled robots for autonomous SCGM and for massage of the upper and lower extremities, including massage of the elbow and knee joints, and neck haven't found.

We presented the novel approach to the creation of intelligence self-propelled autonomous portable massage robot for SCGM for back and chest, and for massage of the upper and lower extremities, including massage of the elbow and knee joints, and neck based on original planar spatial parallel mechanisms. The proposed novel concepts of SCGM robot, called the Triangle, and the Octahedral dodekapod can be used in physiotherapy offices, hospitals, rehabilitation, sports and Wellness centers, as well as at home to conduct autonomous self-massage hard to reach areas of the body.

The use of the Triangle and the Octahedral dodekapod will allow you to automate the processes of SCGM and massage of the upper and lower extremities, including massage of the elbow and knee joints, and neck to improve its efficiency and reduce physical weariness and fatigue of therapist. Thus it's possible additional installation of sensors



at the vertices of the Triangle and the Octahedral dodekapod, e.g. ultrasound, which will allow you to extend the functionality of the massager moving.

The Triangle and the Octahedral dodekapod could be used as future intelligent base blocks for various rehabilitation and other robotic systems that can self-propelled and self-reconfigure.

Current objective is to design software and equip the Triangle and the Octahedral dodekapod with reliable and miniature electronics, linear drives and communication hardware.

Another future task is in applying of the Triangle the Octahedral dodekapod towards on-line diagnostics of patient's health during the rehabilitation procedure.

#### References:

- [1] V. I. Dubrovsky and A. V. Dubrovskaya, *Therapeutic massage*. Moscow: GEOTAR-Media, 2004 (in Russian).
- [2] R. Bischoff, J. Kurth, G. Schreiber, R. Koeppel, A. Albu-Schäffer, A. Beyer, O. Eiberger, S. Haddadin, A. Stemmer, G. Grunwald, and G. Hirzinger, "The KUKA-DLR Lightweight Robot arm-a new reference platform for robotics research and manufacturing," in: *Proceedings of the Robotics (ISR), 2010 41st international symposium on and 2010 6th German conference on robotics (ROBOTIK)*. VDE Verlag GmbH, Berlin, 2011, pp. 741-748.
- [3] J.-P. Merlet, *Parallel Robots*. 2nd ed. Dordrecht: Springer, 2006.
- [4] V. Golovin, M. Arkhipov, and V. Zhuravlev, "Force training for position/force control of massage robots," in *New Trends in Medical and Service Robots*. Springer International Publishing, 2014, pp. 95-107.
- [5] Y. Huang, J. Li, Q. Huang, and C. Liu, "Design and control of anthropomorphic BIT soft arms for TCM remedial massage," in: *Proceedings of the 2013 IEEE/RSJ International Conference on Intelligent Robots and Systems, Tokyo, Japan, November 3-7, 2013*. IEEE, 2013, pp. 1960-1965.
- [6] EMMA, The Robot Therapist. *Innovation - The Singapore Magazine of Research and Technology and Education*, Volume 15, Number 1, 2016, <http://www.innovationmagazine.com/volumes/v15n1/in-brief2.html>
- [7] S. N. Sajapin and M. S. Sajapina, "Movable massaging apparatus and method for giving massage with use thereof," Russian Patent 2 551 939, June 10, 2015.
- [8] S. N. Sajapin, "Adaptive mobile spatial rehabilitation robotic arm and method of facilitating movements and diagnosis of patient using same," Russian Patent 2 564 754, October 10, 2015.
- [9] A. Sh. Koliskor, "Development and study of industrial robots based on *l*-coordinates," *Stanki i Instrument*, no 12, pp. 21-24, December 1982 (in Russian).
- [10] R. Belisle, C. H. Yu, R. Nagpal, "Mechanical Design and Locomotion of Modular-Expanding Robots," in: *Proceedings of the 2010 IEEE International Conference on Robotics and Automation, Anchorage, USA, May 3-8, 2010*. IEEE, 2010, pp. 17-23.
- [11] S. N. Sajapin and A. V. Sinev, "Adaptive mobile 3D manipulator robot and method of organising displacements and control over physical mechanical properties, geometrical shape of contact surface and displacement trajectory hereby," Russian Patent 2 564 754, July 27, 2011.
- [12] S. N. Sayapin, Parallel Spatial Robots of Dodecapod Type, *Journal of Machinery Manufacture and Reliability*, Vol. 41, No. 6, 2012, pp. 457-466.